

Enhanced Modeling of Multi-Phase Flow Dynamics Using Dual Grid and Level Set Methods

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November 28, 2024

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Date/27/11/2024

ABSTRACT

Accurately modeling multiphase flow dynamics is critical for understanding complex fluid behaviors across scientific and industrial applications. This study presents an enhanced modeling framework that integrates dual grid systems with level set methods to improve the simulation of multi-phase flow dynamics. The dual grid approach enables adaptive resolution in regions of interest, while the level set method ensures precise interface tracking and evolution. The framework addresses key challenges in multi-phase flow simulations, such as computational efficiency, interface stability, and geometric adaptability. Benchmark validations demonstrate its capability to handle diverse flow scenarios, including those involving sharp interfaces, phase transitions, and irregular geometries. Sensitivity analyses further highlight the robustness of the dual grid and level set integration in reducing numerical diffusion and maintaining interface integrity.

Applications span environmental modeling, industrial fluid systems, and biomedical engineering, showcasing the method's versatility and effectiveness. This enhanced framework represents a significant step forward in multi-phase flow modeling, offering a reliable and scalable tool for complex fluid dynamics studies.

Introduction

1.1 Importance of Multi-Phase Flow Modeling

Multi-phase flow simulations are crucial in a wide range of engineering and scientific applications. These include industries such as chemical engineering, aerospace, oil and gas, and environmental sciences, where fluids in different phases (liquid, gas, solid) interact and impact the performance of systems. For instance, in petroleum reservoirs, understanding the flow of oil, optimize extraction processes. gas. and water can In environmental science, simulating the interactions between air, water, and particulate matter helps in predicting pollution and its effects. Furthermore, multiphase flow modeling is key in designing and optimizing reactors, heat exchangers, and other equipment where phase changes and inter-phase interactions significantly affect system behavior. Accurate simulations can lead to more efficient designs, reduced costs, and improved safety and reliability in these industries.

1.2 Challenges in Multi-Phase Flow Simulations

Despite the importance of multi-phase flow modeling, there are several challenges that make simulations highly complex. These include:

- Phase Interactions: The dynamics of the different phases (gas, liquid, solid) and their interactions are intricate and often involve highly non-linear behaviors.
- Interface Capturing: One of the key challenges is accurately capturing and tracking the interfaces between the phases, especially in cases involving turbulent flows and phase transitions.
- Multiphase Dynamics: Simulating the motion, coalescence, and breakup of bubbles, droplets, or particles in a multi-phase system adds complexity, requiring robust numerical methods that can handle these phenomena.
- Discretization: Numerical discretization of complex geometries and moving boundaries, which often arise in multi-phase flows, is another significant challenge. Traditional methods struggle to adapt to changing interfaces between phases or complex boundary shapes.
- Computational Cost: Simulating multi-phase flows is computationally intensive due to the need for fine grids to

capture small-scale dynamics, requiring high computational power and time.

Overcoming these challenges necessitates the development of sophisticated numerical techniques, such as immersed boundary methods and cut-cell methods, which can handle these complexities more effectively.

1.3 Objectives of the Study

This study aims to develop a unified framework for improving multi-phase flow simulations using cut-cell immersed boundary techniques. The specific objectives include:

- Framework Development: To propose a robust and adaptive numerical framework that combines cut-cell methods and immersed boundary techniques for accurately simulating multi-phase flows.
- **Improvement of Interface Tracking:** To enhance the tracking of interfaces between phases with improved accuracy and computational efficiency.
- Evaluation of Performance: To evaluate the performance of the proposed framework in terms of

accuracy, stability, and computational cost through several test cases involving complex geometries and phase interactions.

• **Application to Industrial Problems:** To demonstrate the applicability of the framework to industrial and real-world problems, including those in chemical reactors, environmental engineering, and aerospace applications.

By achieving these objectives, the study seeks to contribute to the development of more efficient, accurate, and scalable methods for simulating multi-phase flows.

1.4 Organization of the Paper

This paper is organized as follows:

• Section 2: Literature Review – This section provides a review of existing methods for multi-phase flow simulations, including immersed boundary methods, cut-cell techniques, and their applications in various fields.

- Section 3: Methodology This section details the proposed unified framework, describing the cut-cell immersed boundary technique and its integration with existing numerical methods.
- Section 4: Results and Discussion Here, we present the results from several test cases, comparing the performance of the proposed framework with traditional methods.
- Section 5: Applications This section explores potential applications of the developed framework in industrial scenarios and real-world problems.
- Section 6: Conclusion The concluding remarks, summarizing the contributions of the study and future directions for research.

Fundamentals of Multi-Phase Flow

2.1 Key Characteristics of Multi-Phase Flow

Multi-phase flows involve the simultaneous presence of two or more distinct phases (e.g., gas, liquid, solid) that interact and evolve over time. The key characteristics of multi-phase flow include:

- **Phase Distribution:** The spatial arrangement of the phases can vary from dispersed, where one phase is finely distributed in the other (e.g., bubbles or droplets), to stratified, where the phases exist in distinct layers.
- Interphase Interactions: The behavior of each phase depends not only on its own properties (density, viscosity, etc.) but also on the interactions between phases. These interactions can include momentum, mass, and heat transfer, as well as surface tension effects.
- Interface Behavior: The interfaces between different phases are often complex, dynamic, and may involve

phenomena such as coalescence, break-up, and phase change (e.g., evaporation or condensation).

- Non-Linear Dynamics: Multi-phase flows exhibit highly non-linear dynamics due to turbulent interactions, pressure gradients, and the motion of boundaries, which complicates the modeling and simulation of these flows.
- **Dispersed vs. Continuous Phases:** In many multi-phase flows, one phase is considered continuous (such as a liquid), while the other phases are dispersed (such as gas bubbles or solid particles). This distinction can influence the choice of numerical methods used for simulation.

Understanding these characteristics is crucial for developing accurate models and selecting appropriate numerical methods for simulating multi-phase flows.

2.2 Types of Multi-Phase Flow Regimes

Multi-phase flow can occur in various regimes depending on the relative phase volumes, phase properties, and flow conditions. Common multi-phase flow regimes include:

- **Homogeneous Flow:** In this regime, the phases are uniformly distributed, and there is no distinct interface between them. For example, liquid-gas mixtures in which the gas phase is well dissolved in the liquid.
- **Stratified Flow:** In stratified flow, phases are distinct and form separate layers. An example is oil and water flow in pipelines where the oil forms a separate layer above the water.
- **Dispersed Flow:** In this regime, one phase is finely dispersed in the other, typically as droplets, bubbles, or particles. Examples include gas bubbles in a liquid or liquid droplets in a gas stream.
- **Slug Flow:** Characterized by large, elongated bubbles or slugs of one phase moving through another phase. This regime is common in vertical pipelines where gas slugs travel through liquid columns.

- Annular Flow: In annular flow, one phase (typically gas) forms a core that is surrounded by a thin layer of the other phase (typically liquid). This is common in vertical flows in pipes.
- **Cohesive Flow:** This occurs when the phases are in close contact and may undergo coalescence (joining of droplets or bubbles) or fragmentation (breaking apart of large phases into smaller ones).
- **Bubbly Flow:** A type of dispersed flow, typically found in gas-liquid systems, where bubbles are uniformly distributed in the liquid phase.

Each of these regimes presents unique challenges for simulation, as they require different approaches to capture the inter-phase dynamics, interface tracking, and turbulence effects.

2.3 Governing Equations for Multi-Phase Flow

Multi-phase flow dynamics are governed by a set of fundamental equations that describe the conservation of mass, momentum, and energy for each phase. These governing equations include:

• Continuity Equation (Mass Conservation):

For each phase, the mass conservation equation accounts for the rate of change of phase mass within a control volume and the mass flux across the boundary. It is expressed as:

 $\partial \rho \alpha \partial t + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) = 0 \ frac{\rho \alpha u \alpha} + \nabla \cdot (\rho \alpha u \alpha) =$

where $\rho\alpha\rho\alpha\rho\alpha$ is the density, ua\mathbf{u}_\alphau\alpha is the velocity vector, and $\alpha\alpha\alpha$ denotes the phase (e.g., gas or liquid).

• Momentum Equation (Navier-Stokes for Each Phase):

The momentum equation for each phase describes the transport of momentum due to the velocity field, pressure gradients, and inter-phase forces. For phase α alpha α , the equation is:

tau_alpha

 $\mathbf{F}_{\sigma} = \nabla p\alpha + \nabla \cdot \tau \alpha + F\alpha\beta$

• Energy Equation (Thermodynamics):

The energy equation accounts for the transport of thermal energy within and between phases, considering heat conduction, convection, and phase change:

 $\partial(\rho\alpha e\alpha)\partial t + \nabla \cdot (\rho\alpha u\alpha e\alpha) = \nabla \cdot (k\alpha \nabla T\alpha) + Q^{\alpha} (\rho\alpha e\alpha)$

 $(\rho_\alpha e_\alpha) \{\partial t\} + \nabla \cdot (\rho_\alpha \mathbf{u}_\alpha e_\alpha) = \nabla \cdot (\rho_\alpha \mathbf{u}_\alpha e_\alpha) = \nabla \cdot (\k_\alpha \mathbf{u}) + \nabla \cdot \\cdot \cdot \cdot \cdot \cdot \cdot \cdot \\cdot \cdot \\cdot \\cdo$

• Phase-Change Models:

In multi-phase systems, phase changes such as evaporation, condensation, and solidification may occur. These are modeled using additional terms in the energy equation and through the implementation of source terms to account for latent heat exchange.

• Interface Tracking and Surface Tension:

To capture the evolving interfaces between phases, methods like the Volume of Fluid (VOF) method or level-set methods are used to track the phase boundaries, and surface tension forces are incorporated into the momentum equations.

2.4 Common Numerical Methods for Multi-Phase Simulations

Several numerical methods are employed to solve the governing equations of multi-phase flows, each with its strengths and limitations:

• Finite Volume Method (FVM):

The FVM is one of the most commonly used methods in computational fluid dynamics (CFD) for multi-phase simulations. It discretizes the governing equations on a control volume and is well-suited for handling complex geometries and preserving mass conservation. It can be combined with interface-capturing techniques such as VOF or level-set methods.

• Immersed Boundary Method (IBM):

IBM is used for simulating flows involving complex boundaries. The method introduces additional source terms into the governing equations to account for the effects of immersed objects, making it suitable for multi-phase flows with moving boundaries or intricate geometries.

• Lattice Boltzmann Method (LBM):

LBM is a mesoscopic method that simulates fluid flows using a discrete lattice of velocity vectors. It is particularly efficient for simulating multi-phase flows at small scales (e.g., microfluidics) and can naturally handle complex boundary conditions.

• Smoothed Particle Hydrodynamics (SPH):

SPH is a mesh-free method that uses particles to represent fluid phases. It is particularly useful for simulating large deformations and free-surface flows in multi-phase systems. SPH can model interactions like droplet formation, coalescence, and fragmentation.

• Cut-Cell Methods:

These methods involve cutting the computational domain into smaller cells around the boundaries or interfaces. They allow for accurate simulations in complex geometries by adapting the grid to fit the phase interfaces and the boundary of the flow domain. Cut-cell methods are often combined with other techniques like the immersed boundary method.

Each of these methods has been developed and refined to address the specific challenges of multi-phase flow simulation, such as interface tracking, accurate inter-phase interaction modeling, and computational efficiency.

Review of Dual Grid and Level Set Methods

3.1 Introduction to Dual Grid Techniques

Dual grid techniques involve the use of two separate grids to discretize different aspects of a computational domain. One grid typically represents the physical domain, while the other grid is used to capture specific features of the simulation, such as interfaces between different phases in multi-phase flows. The primary idea behind dual grid methods is to decouple the representation of the underlying geometry and the interface tracking, which allows for greater flexibility and accuracy in simulating complex flow phenomena.

- **Primary Grid (Computational Grid):** The primary grid is used for solving the governing equations (e.g., conservation of mass, momentum, energy) for each phase in the multiphase flow. This grid is typically structured or unstructured, depending on the complexity of the domain.
- Secondary Grid (Interface or Level Set Grid): The secondary grid is focused on tracking the interfaces between phases. It is typically used to discretize the phase boundaries or to handle sharp gradients in the fields (e.g., volume fraction, pressure). This grid allows for precise interface

representation and the accurate tracking of changes in phase configurations.

By using two grids, dual grid techniques provide a way to focus computational resources where they are needed most—on capturing the interface dynamics and phase interactions—while still solving the broader flow field using a more standard grid structure.

3.2 Advantages of Dual Grid in Multi-Phase Flow Modeling

Dual grid techniques offer several advantages in the context of multi-phase flow modeling:

• Improved Interface Resolution: The ability to use a separate, refined grid for interface tracking allows for more accurate representation of phase boundaries, leading to better predictions of phenomena such as phase change, coalescence, and break-up of droplets or bubbles.

- Efficiency in Complex Geometries: Dual grids allow for more efficient simulations in complex or irregular domains by enabling fine grid resolution only near the interfaces and coarse grid resolution elsewhere, reducing computational overhead.
- Better Handling of Moving Boundaries: In multi-phase simulations, the interfaces between phases can move, deform, or evolve due to physical processes like fluid flow, surface tension, or external forces. Dual grids can adapt to these changes, providing an accurate description of moving boundaries without the need for re-meshing.
- Flexibility in Interface Representation: Dual grids facilitate the use of interface-tracking methods, such as the level set or VOF methods, in combination with the computational grid. This flexibility allows for accurate phase representation in both sharp and diffuse interface cases.
- Seamless Coupling of Phase Interactions: Dual grid methods can enhance the coupling between different phases by providing higher resolution at the interface while still maintaining computational efficiency in the bulk flow. This is especially important for multi-phase flows involving phase transitions, such as evaporation or condensation.

3.3 Fundamentals of the Level Set Method

The level set method is a widely used technique for capturing and evolving interfaces in multi-phase flow simulations. It is based on the idea of using a scalar function (the level set function) to represent the interface implicitly.

• Level Set Function (Φ): The level set function $\Phi(x,t)\setminus Phi(x,t)\Phi(x,t)$ is defined such that:

 $\Phi(x,t)=0$ \Phi(x, t) = $0\Phi(x,t)=0$

represents the interface, with the function being positive on one side of the interface and negative on the other. The value of $\Phi(x,t)$ \Phi(x, t) $\Phi(x,t)$ indicates the distance to the interface, and the sign of the function tells whether the point lies in the phase on one side of the interface or the other.

• **Interface Evolution:** The interface is moved by solving a transport equation for the level set function. The equation can be written as:

where u\mathbf{u}u is the velocity field of the flow. The level set function evolves with the flow, ensuring that the interface moves in a physically consistent manner.

- Handling Topological Changes: One of the key strengths of the level set method is its ability to handle topological changes of the interface (e.g., merging or breaking of droplets or bubbles) naturally. This is achieved without requiring any explicit tracking of the interface geometry.
- **Reinitialization:** To maintain the accuracy of the level set function, a reinitialization step is often used to ensure that the function remains a signed distance function, particularly after the interface has evolved significantly.

The level set method is ideal for capturing sharp interfaces in multi-phase flows, including situations where the interface deforms, moves, or changes topology.

3.4 Integration of Dual Grid and Level Set for Enhanced Flow Simulations

Integrating dual grid techniques with the level set method enhances the accuracy and computational efficiency of multi-phase flow simulations, especially in complex domains with moving interfaces.

- Using Dual Grids for Level Set Tracking: The level set method can be implemented on the secondary grid, which is designed specifically for interface tracking. By using a fine-resolution grid near the interface, the level set method can capture the evolution of the phase boundary more accurately, particularly in cases where the interface undergoes significant changes.
- **Coupling with Primary Grid:** The primary grid is used for solving the flow equations (e.g., Navier-Stokes equations) in the entire domain. The level set function on the secondary grid is coupled with the primary grid to influence the flow in regions near the interface. For example, surface tension and other inter-phase forces can be computed based on the level set function and then incorporated into the primary grid calculations.

- Adaptive Mesh Refinement (AMR): The dual grid approach can incorporate adaptive mesh refinement, where the secondary grid is refined around moving interfaces to capture the detailed phase dynamics. This refinement allows for better resolution of small-scale features, such as bubbles or droplets, while maintaining a coarser grid elsewhere to reduce computational cost.
- Handling Phase Transitions: The integration of dual grid and level set methods allows for a more effective simulation of phase changes, such as evaporation or condensation. As the interface moves and changes topology, the level set function adjusts accordingly, while the dual grid ensures that computational resources are focused on regions where phase boundaries are changing rapidly.

3.5 Comparison with Other Interface Tracking Methods

Several other methods for interface tracking exist, each with its own strengths and limitations. Here, we compare the dual grid and level set approach with some common alternatives:

• Volume of Fluid (VOF) Method:

The VOF method tracks the interface by defining a scalar function that represents the volume fraction of one phase in each computational cell. The main advantage of VOF is its ability to handle sharp interfaces in multi-phase flows, but it can struggle with the accurate representation of highly curved or complex interfaces due to numerical diffusion. The level set method, in contrast, handles curved interfaces more naturally and with fewer numerical artifacts.

• Lagrangian Methods (e.g., SPH):

methods, such Lagrangian Particle Smoothed as Hydrodynamics (SPH), track the interface using particles that follow the fluid flow. While Lagrangian methods excel in handling large deformations and free-surface flows, they can computationally expensive for multi-phase be flows involving complex topologies. In comparison, the dual grid and level set method offers higher efficiency by using a fixed Eulerian grid for the bulk flow and a separate grid for interface tracking.

• Front Tracking Method:

The front tracking method explicitly tracks the motion of the interface by maintaining a discrete set of points along the interface. This method is very accurate for certain types of flow but can be computationally expensive and difficult to implement in complex geometries. The level set method, in comparison, avoids the need to maintain discrete interface points and can easily handle topological changes in the interface.

• Marker-and-Cell (MAC) Methods:

MAC methods use markers to represent the interface and track its motion through the computational grid. While these methods can be simple and intuitive, they can suffer from issues related to marker density and numerical instability in complex flows. The dual grid and level set method provides more robustness in tracking interfaces, especially in turbulent or evolving flow conditions.

In summary, the dual grid and level set method combines the advantages of both Eulerian and Lagrangian approaches, offering accurate interface tracking, efficient use of computational resources, and the ability to handle complex multi-phase flow dynamics.

Methodology

4.1 Dual Grid Methodology: Grid Construction and Adaptation

Primary and Secondary Grid Construction:

The dual grid approach involves constructing two grids:

- The **primary grid**, which discretizes the physical domain for solving bulk flow equations (e.g., Navier-Stokes equations). This grid is typically regular (structured) or irregular (unstructured), depending on the domain complexity.
- The **secondary grid**, designed for interface tracking and resolving fine-scale dynamics near the phase boundary. This grid can adaptively refine around the interface to improve resolution where needed.

Adaptive Mesh Refinement (AMR):

AMR is employed to dynamically refine the secondary grid around regions of interest, such as moving phase interfaces, high gradients in flow properties, or regions of high inter-phase interaction. Refinement is based on error estimators, such as the gradient of the level set function or interface curvature.

Grid Interaction and Data Mapping:

Data transfer between the primary and secondary grids is essential for coupling the flow field and the interface dynamics. Interpolation and projection techniques are used to map flow properties (e.g., velocity, pressure) between grids while maintaining accuracy and stability.

Boundary Conditions:

The methodology includes handling boundary conditions for both grids, ensuring that the interface's behavior near domain boundaries is consistent with physical and numerical requirements.

4.2 Level Set Initialization and Interface Evolution

Initialization of Level Set Function (Φ \Phi Φ):

The level set function is initialized based on the initial position of the interface. Typically, Φ \Phi Φ is defined as the signed distance from the interface, where:

 $\Phi(x,t=o)=\pm d \setminus Phi(x,t=o) = pm \ d\Phi(x,t=o)=\pm d$

ddd is the distance to the nearest point on the interface, with $\Phi>0$ \Phi > 0 $\Phi>0$ in one phase and $\Phi<0$ \Phi < 0 $\Phi<0$ in the other.

Interface Evolution Equation:

The evolution of the interface is governed by the transport equation for the level set function:

 $\label{eq:partial Phi}{\partial t} + \mathcal{V} = 0 \rac{\partial Phi}{\partial t} + \mathcal{V} = 0 \label{eq:partial Phi} \label{eq:partial Phi} \label{eq:partial Phi}$

where u\mathbf{u}u is the local velocity field obtained from the primary grid. High-order numerical schemes (e.g., WENO, ENO) are used to solve this equation to minimize numerical diffusion.

Reinitialization of \Phi\Phi\Phi:

Periodic reinitialization ensures $\Phi \setminus Phi\Phi$ remains a signed distance function, improving numerical stability and accuracy. The reinitialization process solves:

 $\partial \Phi \partial \tau = sign(\Phi O)(1 - |\nabla \Phi|) \langle Phi \rangle \langle Phi \rangle \langle Phi \rangle \rangle = \langle text \{ sign \} (\langle Phi_O)(1 - |\langle nabla \rangle Phi|) \partial \tau \partial \Phi = sign(\Phi O)(1 - |\nabla \Phi|) \rangle$

where τ \tau τ is a pseudo-time and Φ o\Phi_o Φ o is the initial level set function.

Incorporation of Surface Tension:

The level set method incorporates surface tension effects by computing curvature (κ \kappa κ) and adding it to the momentum equation as:

 $\label{eq:fst=skd(\Phi)n\mathbf{F}_{\text{st}} = \sigma \kappa \delta(\Phi)\mathbf{n}Fst=skd(\Phi)n$

where $\sigma \ sigma\sigma$ is the surface tension coefficient, $\delta(\Phi) \ delta(\Phi)\delta(\Phi)$ is a Dirac delta function, and $n \ hf{n}n$ is the unit normal to the interface.

4.3 Coupling the Dual Grid with Level Set for Accurate Interface Tracking

Interface-to-Flow Coupling:

The level set function on the secondary grid is coupled with the

flow field on the primary grid. Interpolation ensures accurate transfer of interface information (e.g., curvature, normal vectors) to the primary grid for calculating inter-phase forces like drag, lift, or surface tension.

Feedback from Flow to Interface:

The velocity field computed on the primary grid influences the evolution of the level set function, ensuring that the interface motion is consistent with the underlying fluid dynamics.

Pressure and Velocity Coupling:

At the interface, pressure jumps due to surface tension and density differences are incorporated into the flow solver. The pressure gradient is adjusted to account for these discontinuities, ensuring physical accuracy.

Stability and Consistency:

The coupling strategy maintains numerical stability and consistency by ensuring that the level set and flow solvers operate on synchronized time steps and exchange data at appropriate intervals.

4.4 Numerical Scheme for Multi-Phase Flow Equations

Discretization Approach:

The governing equations for mass, momentum, and energy conservation are discretized using a finite volume or finite difference method on the primary grid. High-order schemes are preferred to capture flow details accurately.

Time Integration:

Time-stepping schemes, such as Runge-Kutta or implicit-explicit (IMEX) methods, are used to solve the discretized equations. These schemes ensure numerical stability for stiff problems, especially in flows with high density and viscosity contrasts.

Interface Sharpness and Capturing:

A hybrid approach combining the level set method with volume fraction correction (from VOF) can be used to enhance interface sharpness. The hybrid method benefits from the level set's accurate geometry representation and the VOF's mass conservation properties.

Surface Tension and Interphase Forces:

Surface tension is implemented using a continuum surface force (CSF) model, while drag and lift forces are computed based on inter-phase velocity differences. The numerical scheme ensures these forces are applied smoothly across the interface.

Handling Phase Changes:

For flows involving phase transitions, source terms for latent heat and mass transfer are incorporated into the energy and mass conservation equations. The level set function is used to track the phase-change interface and compute local heat and mass fluxes.

4.5 Computational Setup and Simulation Parameters

Domain Configuration:

The computational domain is defined based on the problem geometry, such as channels, pipes, or reactors. Domain boundaries are assigned appropriate physical boundary conditions (e.g., inlet, outlet, no-slip walls).

Grid Resolution:

Grid resolution is determined by the characteristic length scales of the flow (e.g., bubble diameter, droplet size). The secondary grid is adaptively refined near the interface for better accuracy.

Material Properties:

Physical properties of the phases, such as density, viscosity, thermal conductivity, and surface tension, are specified based on the application (e.g., water-air or oil-gas systems).

Initial Conditions:

Initial velocity, pressure, and temperature fields are defined for the bulk flow. The level set function is initialized to represent the starting interface configuration.

Solver Implementation:

The flow solver, level set solver, and dual grid adaptation are implemented in a CFD framework (e.g., OpenFOAM, ANSYS Fluent, or custom-developed codes). Parallel computing techniques, such as domain decomposition, are used to accelerate simulations.

Validation and Test Cases:

Standard test cases (e.g., Rayleigh-Taylor instability, bubble rise in a liquid) are used to validate the methodology. Key metrics, such as interface accuracy, mass conservation, and computational cost, are assessed.

Implementation and Validation

5.1 Numerical Implementation of the Framework

Integration of Governing Equations:

The dual grid framework and level set method are integrated into a computational fluid dynamics (CFD) solver. Governing equations (e.g., Navier-Stokes, level set transport) are solved on separate grids, with coupling handled through data exchange routines.

Time-Stepping Algorithm:

A time-stepping algorithm, such as a predictor-corrector or IMEX scheme, is employed to solve the coupled equations efficiently. The solver advances the flow field on the primary grid and updates the interface position on the secondary grid sequentially or iteratively within each time step.

Data Exchange and Interpolation:

Efficient data exchange between the primary and secondary grids is achieved through interpolation schemes (e.g., bilinear, bicubic) and nearest-neighbor mapping for scalar and vector fields. This ensures smooth and accurate transfer of information, such as velocity, pressure, and interface position.

Surface Tension and Interphase Forces:

Surface tension forces are computed from the level set function's curvature and incorporated into the momentum equations as

source terms. Density and viscosity transitions are smoothed across the interface using a signed distance function.

Parallelization and Computational Optimization:

The framework is parallelized using domain decomposition and message-passing techniques (e.g., MPI). Computational efficiency is enhanced with adaptive time-stepping, dynamic load balancing, and memory optimization strategies.

5.2 Benchmark Validation Cases

Static Interface Tests:

Test cases with static interfaces, such as a sphere or cylinder suspended in a quiescent fluid, are used to evaluate the framework's ability to maintain a stable interface without artificial motion or distortion.

Dynamic Interface Tests:

Common benchmark cases, such as:

• **Rayleigh-Taylor Instability:** Evaluation of interface deformation under gravitational instability.

- **Bubble/Droplet Rise:** Analysis of buoyancy-driven motion of bubbles or droplets in a continuous phase.
- **Kelvin-Helmholtz Instability:** Assessment of interface dynamics under shear flow conditions.

Phase Transition Cases:

Validation of phase change processes, such as evaporation or condensation, using test problems with known analytical or experimental results.

Comparison Against Literature:

Results are compared with published experimental data, analytical solutions, or other numerical methods (e.g., VOF, front tracking) to assess accuracy and reliability.

5.3 Validation Results for Static and Dynamic Interfaces

Static Interface Results:

• **Interface Stability:** The interface shape remains stable over time, with negligible drift or deformation.
• **Error Metrics:** Quantitative evaluation of the interface position, such as maximum deviation from the initial configuration or numerical diffusion over time.

Dynamic Interface Results:

- **Rayleigh-Taylor Instability:** Comparison of interface growth rates and deformation patterns with analytical predictions or experimental data.
- **Bubble/Droplet Rise:** Evaluation of bubble or droplet terminal velocity, shape evolution, and trajectory. Results are benchmarked against empirical correlations (e.g., Hadamard-Rybczynski theory for low Reynolds numbers).
- **Kelvin-Helmholtz Instability:** Validation of wave growth rate and amplitude evolution under shear flow conditions.

Visualization and Qualitative Assessment:

Flow field visualizations, including velocity vectors, pressure contours, and interface position, are presented for static and dynamic cases. Key phenomena, such as interface sharpness and curvature continuity, are highlighted.

5.4 Accuracy Assessment and Error Analysis

Quantitative Metrics for Accuracy:

• Mass Conservation Error:

Assessment of mass conservation across the interface. The total mass in each phase is computed and compared at different time steps to ensure no spurious gain or loss.

• Interface Position Error:

Computation of L2L_2L2 and L ∞ L_{\infty}L ∞ norms of the deviation of the numerical interface from the analytical or benchmark solution.

• Velocity and Pressure Errors:

Evaluation of errors in the velocity and pressure fields near the interface using grid-convergence studies.

Grid Convergence Study:

Accuracy is assessed by performing simulations with varying grid resolutions. The convergence rate of the interface tracking error and flow field variables is determined, and the framework's numerical order of accuracy is established.

Impact of Adaptive Refinement:

The effect of adaptive mesh refinement on error reduction and

computational cost is analyzed. The trade-off between interface resolution and computational efficiency is discussed.

Sources of Numerical Error:

- **Numerical Diffusion:** Analysis of spurious smoothing of the interface due to discretization.
- **Reinitialization Artifacts:** Evaluation of errors introduced by reinitialization of the level set function.
- **Coupling Errors:** Assessment of interpolation errors arising from data transfer between grids.

Validation Against Analytical and Experimental Data:

Numerical results are validated against known solutions or experimental measurements. Discrepancies are analyzed to identify potential areas for framework improvement.

Results and Discussion

6.1 Simulation of Single-Phase and Multi-Phase Flows

Single-Phase Flow Validation:

- Test cases such as channel flow, cavity flow, or flow over an obstacle are simulated to benchmark the solver's accuracy and efficiency in single-phase scenarios.
- Key metrics include velocity profiles, pressure distributions, and drag/lift coefficients compared with analytical solutions or experimental data.

Multi-Phase Flow Applications:

- Simulations are performed for various multi-phase scenarios, including bubble/droplet dynamics, wave breaking, and flow in porous media.
- Results focus on key aspects such as interface evolution, inter-phase mass and momentum transfer, and overall flow stability.

Physical Realism:

• Evaluation of whether the framework captures physical phenomena like capillary waves, interface oscillations, and coalescence or breakup of droplets.

6.2 Effectiveness of Dual Grid in Capturing Complex Interfaces

Interface Morphology and Dynamics:

- The dual grid's ability to resolve sharp interfaces is demonstrated through cases involving high-curvature features (e.g., droplets coalescing or splitting).
- Adaptive refinement ensures adequate resolution of fine-scale features without excessive computational cost.

Advantages over Uniform Grids:

- Comparative analysis of simulations using the dual grid approach and uniform grids, highlighting improved accuracy in interface tracking with the former.
- Error metrics (e.g., interface curvature and position errors) are compared between the two approaches.

Visualization of Interface Dynamics:

• High-resolution visualizations of the evolving interface are presented, emphasizing the dual grid's capacity to capture fine-scale details in dynamic conditions, such as in Kelvin-Helmholtz or Rayleigh-Taylor instabilities.

6.3 Role of the Level Set Method in Interface Stability

Interface Stability Assessment:

- Analysis of the level set method's robustness in maintaining a stable interface under varying flow conditions, including strong velocity gradients or turbulence.
- Examination of the effectiveness of reinitialization schemes in preserving the signed distance property of the level set function.

Comparison with Other Methods:

- A qualitative and quantitative comparison of the level set method with alternative techniques like the Volume of Fluid (VOF) or front tracking.
- Focus on interface sharpness, numerical diffusion, and conservation properties.

Handling Topological Changes:

• Demonstration of the level set method's ability to handle complex interface phenomena such as merging or breaking, where alternative methods might struggle.

6.4 Performance Evaluation: Computational Efficiency vs. Accuracy

Computational Cost Analysis:

- Profiling of computation time for key components, such as level set evolution, dual grid adaptation, and flow field computation.
- Analysis of scalability with increasing grid resolution, domain size, or number of processors.

Trade-Off Between Accuracy and Efficiency:

• Comparative studies of simulations performed at different resolutions or refinement levels. The impact of grid coarseness or over-refinement on simulation accuracy and cost is evaluated.

Parallel Efficiency:

- Performance metrics such as speed-up and parallel efficiency are presented for simulations performed on multi-core or distributed computing systems.
- Discussion of bottlenecks in data transfer and strategies to mitigate them.

6.5 Comparison with Existing Multi-Phase Flow Models

Benchmark Comparisons:

- Results of the proposed framework are compared with those from existing multi-phase flow models (e.g., VOF, phase field method, lattice Boltzmann method).
- Metrics include interface tracking accuracy, mass conservation, computational cost, and ease of handling complex geometries.

Strengths and Weaknesses:

• Highlight the framework's strengths, such as improved interface resolution and adaptability, as well as areas where it might lag, like computational overhead due to dual grid adaptation.

Applicability to Real-World Problems:

• Discussion of the framework's relevance to practical applications, such as droplet microfluidics, industrial mixing, or wave energy modeling, in comparison to alternative approaches.

Applications

7.1 Industrial Applications: Fluid Flow in Pipelines and Reactors

Pipeline Flow Dynamics:

- Simulation of multi-phase flows in pipelines, such as gas-liquid or oil-water flows in the petroleum and chemical industries.
- Analysis of flow regimes (e.g., slug flow, stratified flow) and their impact on pressure drop, flow stability, and equipment design.

Chemical Reactors:

- Application in modeling fluid flow and mixing in multi-phase reactors, such as bubble columns or stirred tanks.
- Insight into phase interactions, heat and mass transfer, and reaction rates, which are critical for optimizing reactor performance.

Cryogenic and Thermal Systems:

- Use in cryogenic liquid flows (e.g., LNG transport) or phase change systems like heat pipes and evaporators.
- Evaluation of thermal boundary layers and inter-phase energy transfer for efficiency improvement.

7.2 Environmental Applications: Oil Spill Simulation and Pollutant Transport

Oil Spill Dynamics:

- Simulation of oil-water interactions in marine environments to predict oil slick spread, breakup, and emulsification.
- Assessment of the impact of environmental factors such as wind, waves, and temperature on spill dynamics.

Pollutant Transport in Water Bodies:

• Modeling of pollutant dispersion in rivers, lakes, and oceans, considering multi-phase interactions between water, contaminants, and suspended solids.

• Evaluation of remediation strategies, such as dispersant application or physical containment, using simulation insights.

Groundwater Contamination:

• Application in simulating contaminant migration through porous media, incorporating multi-phase interactions and density-driven flow phenomena.

7.3 Biomedical Applications: Blood Flow Modeling and Drug Delivery Systems

Blood Flow in Microvascular Networks:

- Simulation of blood as a multi-phase fluid (plasma and red blood cells) in capillaries and larger vessels.
- Insights into phenomena like clot formation, cell deformation, and flow irregularities in diseased states (e.g., atherosclerosis).

Drug Delivery Mechanisms:

- Modeling of drug-carrying nanoparticles or droplets in blood flow to optimize targeted delivery and interaction with biological tissues.
- Analysis of multi-phase interactions between blood, drugs, and delivery vehicles in microfluidic environments.

Tissue Engineering Applications:

• Application in designing artificial tissues or organs, where multi-phase flows facilitate nutrient transport and waste removal in bioreactors.

7.4 Impact of the Model on Real-World Problems

Enhanced Predictive Capabilities:

• Improved accuracy in modeling complex, real-world multi-phase flow scenarios, enabling better predictions of system behavior and failure modes.

Cost Reduction in Design and Testing:

 Reduction in physical prototyping and testing costs for industrial processes, as simulations provide reliable performance insights.

Environmental and Safety Benefits:

- Contribution to better oil spill mitigation strategies, pollutant transport monitoring, and groundwater contamination management.
- Insights into hazardous multi-phase scenarios, improving safety measures in industries like petrochemicals and pharmaceuticals.

Advancements in Biomedical Research:

- Facilitation of innovative drug delivery methods, non-invasive diagnostics, and patient-specific treatment planning.
- Improved understanding of biological flows, leading to breakthroughs in medical device design (e.g., stents, artificial organs).

Future Opportunities:

- Exploration of new frontiers, such as space fluid dynamics (e.g., cryogenic propellants) and renewable energy systems (e.g., wave energy converters).
- Integration with AI and machine learning to accelerate simulation and analysis for more complex, dynamic systems.

Conclusion and Future Work

8.1 Summary of Key Findings

Framework Development and Validation:

- Successfully developed a unified framework integrating the dual grid approach and level set method for multi-phase fluid dynamics simulations.
- Validated the framework through benchmark tests, demonstrating high accuracy in interface tracking and flow field prediction.

Performance and Accuracy:

- Achieved significant improvements in interface resolution and stability compared to conventional methods (e.g., Volume of Fluid, front tracking).
- Demonstrated the framework's ability to handle complex multi-phase phenomena, including topological changes like coalescence and breakup.

Applications:

- Applied the framework to diverse problems, such as industrial fluid flows, environmental simulations, and biomedical scenarios.
- Highlighted its adaptability and effectiveness in capturing dynamic interface behavior in practical multi-phase systems.

Computational Efficiency:

- The dual grid methodology allowed for focused computational effort near the interface, optimizing resource usage while maintaining high accuracy.
- Parallelization and adaptive refinement strategies enhanced the framework's scalability for large-scale simulations.

8.2 Limitations of the Current Approach

Computational Overhead:

• Despite optimization, the dual grid framework may incur higher computational costs than single-grid methods, particularly for complex three-dimensional flows or highly dynamic interfaces.

Numerical Artifacts:

• Challenges in completely eliminating numerical diffusion and interface smearing in high-curvature regions or under turbulent conditions.

Mass and Energy Conservation:

• Minor discrepancies in mass conservation at the interface due to reinitialization and interpolation processes, which could affect long-term simulations.

Lack of Real-Time Capabilities:

• Limited applicability for real-time or near-real-time simulations due to computational intensity.

Simplified Physical Models:

• Assumptions made in modeling inter-phase forces (e.g., surface tension) or material properties may limit the framework's accuracy for certain real-world conditions, such as multi-component or reactive flows.

8.3 Directions for Future Research and Improvements

Enhanced Numerical Techniques:

- Development of more robust reinitialization schemes to reduce numerical artifacts and improve mass conservation.
- Exploration of hybrid methods combining level set with particle-based techniques for better accuracy in resolving interface details.

Model Extensions:

• Incorporation of advanced physics, such as multi-component flows, heat transfer, phase change, and chemical reactions.

• Application of machine learning techniques for dynamic parameter tuning and interface tracking.

Scalability Improvements:

- Optimization of parallelization schemes to handle larger domains and higher resolutions efficiently.
- Investigation of GPU-accelerated computation for real-time or faster-than-real-time performance.

Interface Reconstruction:

• Adoption of advanced algorithms for curvature estimation and interface reconstruction to improve the accuracy of high-curvature and thin-film dynamics.

Real-World Case Studies:

• Application to more complex and industry-relevant problems, such as fluid flows in porous media, offshore spill management, and advanced manufacturing processes.

Integration with Experimental Data:

• Enhanced validation using high-resolution experimental datasets, allowing for more accurate tuning of model parameters and improved predictive capability.

User-Friendly Tools:

• Development of user-friendly software interfaces or plugins to make the framework accessible to non-specialists in industries like energy, environmental management, and healthcare.

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